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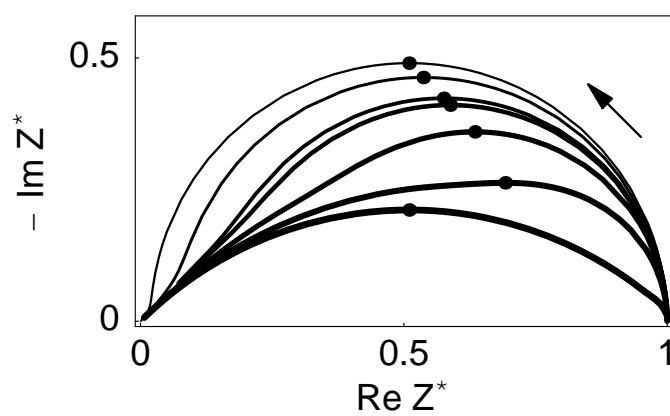


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Handbook  
of  
Electrochemical Impedance Spectroscopy



**DIFFUSION IMPEDANCES**

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July 10, 2020



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# Chapter 1

## Mass transfer by diffusion, Nernst boundary condition

### 1.1 General diffusion equations

From:

$$\frac{\partial \Delta c(x, t)}{\partial t} = D x^{1-d} \frac{\partial}{\partial x} \left( x^{d-1} \frac{\partial \Delta c(x, t)}{\partial x} \right)$$

where  $\Delta$  denotes a small deviation (or excursion) from the initial steady-state value,  $d = 1$  corresponds to a planar electrode,  $d = 2$  to a cylindrical electrode (radial diffusion) and  $d = 3$  to a spherical electrode [5, 33] (Fig. 1.1), it is obtained, using the Nernstian boundary condition  $\Delta c(r_\delta) = 0$ :

$$Z^*(u) \propto \frac{\Delta c(r_0, i u)}{\Delta J(r_0, i u)} = \frac{I_{d/2-1}(\sqrt{i u} \rho) K_{d/2-1}(\sqrt{i u}) - I_{d/2-1}(\sqrt{i u}) K_{d/2-1}(\sqrt{i u} \rho)}{\sqrt{i u} (I_{d/2}(\sqrt{i u}) K_{d/2-1}(\sqrt{i u} \rho) + I_{d/2-1}(\sqrt{i u} \rho) K_{d/2}(\sqrt{i u}))}$$

where  $u$  is a reduced frequency and  $\rho = r_\delta/r_0$ .  $I_n(z)$  gives the modified Bessel function of the first kind and order  $n$  and  $K_n(z)$  gives the modified Bessel function of the second kind and order  $n$  [48].  $I_n(z)$  and  $K_n(z)$  satisfy the differential equation:

$$-y (n^2 + z^2) + z y' + z^2 y'' = 0$$

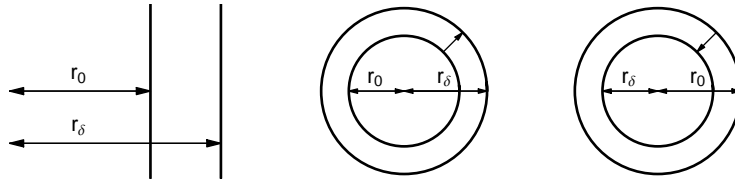


Figure 1.1: Planar diffusion (left), outside [19] (or convex [29]) diffusion ( $\rho = r_\delta/r_0 > 1$ , middle), and central (or concave) diffusion ( $\rho < 1$ , right).

## 1.2 Semi-infinite diffusion

### 1.2.1 Semi-infinite linear diffusion

$$d = 1, \Delta c(\infty) = 0$$

**Impedance** [44, 4]



Figure 1.2: Warburg element [47].

$$Z_W(\omega) = \frac{(1-i)\sigma}{\sqrt{\omega}} = \frac{\sqrt{2}\sigma}{\sqrt{i\omega}}, \quad \text{Re } Z_W(\omega) = \frac{\sigma}{\sqrt{\omega}}, \quad \text{Im } Z_W(\omega) = -\frac{\sigma}{\sqrt{\omega}}$$

$$\sigma = \frac{1}{n^2 F f X^* \sqrt{2 D_X}}, \quad f = \frac{F}{RT}, \quad X^* : \text{bulk concentration, } \sigma \text{ unit: } \Omega \text{ cm}^2 \text{ s}^{-1/2}$$

**Reduced impedance**

$$Z_W^*(u) = Z_W(\omega) = \frac{1}{\sqrt{i}u}, \quad u = \frac{\omega}{2\sigma^2}, \quad \text{Re } Z_W(u) = \frac{1}{\sqrt{2}u}, \quad \text{Im } Z_W(u) = -\frac{1}{\sqrt{2}u}$$

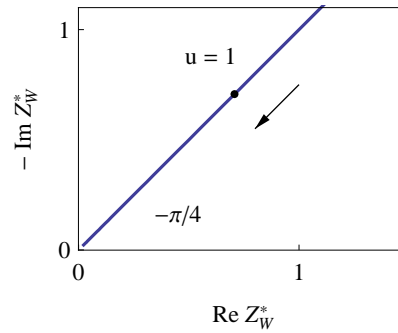


Figure 1.3: Nyquist diagram of the reduced Warburg impedance.

**Randles circuit**

The equivalent circuit in Fig. 1.4 was initially proposed by Randles for a redox reaction  $O + ne \leftrightarrow R$  [38].

$$\sigma = \sigma_O + \sigma_R$$

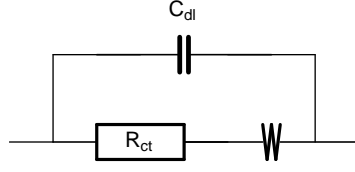


Figure 1.4: Randles circuit for semi-infinite linear diffusion.

**Impedance**

$$Z(\omega) = \frac{1}{i\omega C_{dl} + \frac{1}{R_{ct} + \frac{(1-i)\sigma}{\sqrt{\omega}}}} = \frac{-i((1-i)\sigma + \sqrt{\omega}R_{ct})}{-i\sqrt{\omega} + (1-i)\sigma\omega C_{dl} + \omega^{\frac{3}{2}}C_{dl}R_{ct}}$$

$$\text{Re } Z(\omega) = \frac{\sigma + \sqrt{\omega}R_{ct}}{\sqrt{\omega} \left(1 + 2\sigma\sqrt{\omega}C_{dl} + 2\sigma^2\omega C_{dl}^2 + 2\sigma\omega^{\frac{3}{2}}C_{dl}^2R_{ct} + \omega^2C_{dl}^2R_{ct}^2\right)}$$

$$\text{Im } Z(\omega) = \frac{-\sigma - 2\sigma^2\sqrt{\omega}C_{dl} - 2\sigma\omega C_{dl}R_{ct} - \omega^{\frac{3}{2}}C_{dl}R_{ct}^2}{\sqrt{\omega} \left(1 + 2\sigma\sqrt{\omega}C_{dl} + 2\sigma^2\omega C_{dl}^2 + 2\sigma\omega^{\frac{3}{2}}C_{dl}^2R_{ct} + \omega^2C_{dl}^2R_{ct}^2\right)}$$

**Reduced impedance** "The frequency response of the Randles circuit can be described in terms of two time constants for faradaic ( $\tau_f$ ) and diffusional ( $\tau_d$ ) processes" [46] (Fig. 1.5).

$$Z^*(u) = \frac{Z(u)}{R_{ct}} = \frac{(1+i)T(i+u)}{-T\sqrt{2u} + (1+i)(-1+T+iu)u}$$

$$u = \tau_d\omega, \tau_d = R_{ct}^2/(2\sigma^2), T = \tau_d/\tau_f, \tau_f = R_{ct}C_{dl}$$

$$\text{Re } Z^*(u) = \frac{T^2 \left( -(\sqrt{2}(-1+u)) + 2u^{\frac{3}{2}} \right)}{2\sqrt{2}Tu(1-T+u) + 2\sqrt{u} \left( T^2 + (-1+T)^2u + u^3 \right)}$$

$$\text{Im } Z^*(u) = \frac{T \left( \sqrt{2}T(-1-u) - 2\sqrt{u}(1-T+u^2) \right)}{2\sqrt{2}Tu(1-T+u) + 2\sqrt{u} \left( T^2 + (-1+T)^2u + u^3 \right)}$$

$$\lim_{u \rightarrow 0} \text{Re } Z^*(u) = 1 - \frac{1}{T} + \frac{1}{\sqrt{2}u}, \quad \lim_{u \rightarrow 0} \text{Im } Z^*(u) = -\frac{1}{\sqrt{2}u}$$

**1.2.2 Semi-infinite radial cylindrical diffusion (outside)**

$$d = 2, \Delta c(\infty) = 0$$

$$Z^*(u) = \frac{K_0(\sqrt{iu})}{\sqrt{iu}K_1(\sqrt{iu})}$$

$$\lim_{u \rightarrow 0} -\text{Im } Z^*(u) = \frac{\pi}{4}, \quad \text{Re } Z^*(u_c) = \frac{\pi}{4} \Rightarrow u_c = 0.542$$

(Fig. 1.6)



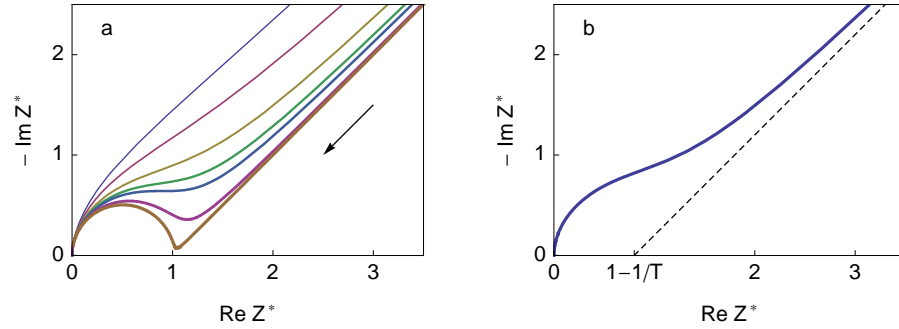


Figure 1.5: a: Nyquist diagram of the reduced impedance for the Randles circuit (Fig. 1.4). Semi-infinite linear diffusion.  $T = 1, 2, 5, 10, 16.4822, 10^2, 10^4$ . Line thickness increases with  $T$ . One apex for  $T > 16.4822$ . The arrows always indicate the increasing frequency direction. b: Extrapolation of the low frequency limit plotted for  $T = 5$ .

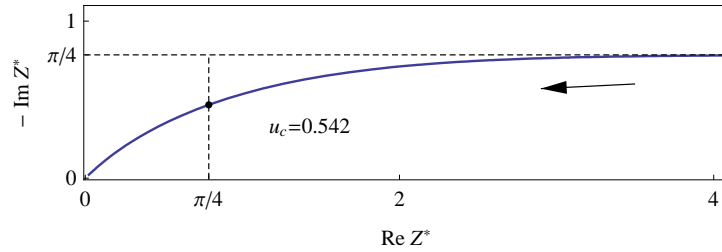


Figure 1.6: Reduced impedance for semi-infinite radial diffusion outside a circular cylinder. Dot: reduced characteristic angular frequency:  $u_c = 0.542$ .

### 1.2.3 Semi-infinite spherical diffusion

$$d = 3, \Delta c(\infty) = 0$$

$$Z^*(u) = \frac{1}{1 + \sqrt{i}u}, \quad u = r_0^2 \omega / D$$

$$\operatorname{Re} Z^*(u) = \frac{2 + \sqrt{2}u}{2(1 + \sqrt{2}u + u)}, \quad \operatorname{Im} Z^*(u) = -\frac{\sqrt{u}}{\sqrt{2}(1 + \sqrt{2}u + u)}$$

(Fig. 1.7)

## 1.3 Bounded diffusion condition (linear diffusion)

$$\Delta c(r_\delta) = 0$$

”Originally derived by Llopis and Colon [26], and subsequently re-derived by Sluyters [42] and Yzermans [50], Drossbach and Schultz [15], and Schuhmann [41]” [4].

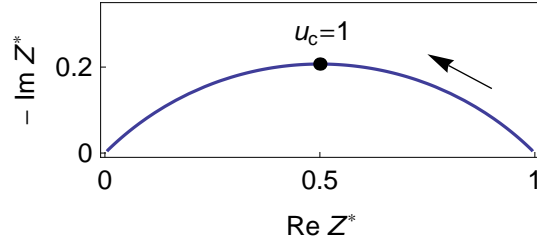


Figure 1.7: Reduced impedance for spherical (outside) diffusion. Dot: reduced characteristic angular frequency:  $u_c = 1$ ,  $\text{Re } Z^*(u_c) = 1/2$ ,  $\text{Im } Z^*(u_c) = (1 - \sqrt{2})/2$ .

- IUPAC terminology: bounded diffusion [43]
- Finite-length diffusion with transmissive boundary condition [22, 28]

$$Z_{W_\delta}^*(u) = \frac{\tanh \sqrt{i}u}{\sqrt{i}u}, \quad u = \tau_d \omega, \quad \tau_d = \delta^2/D, \quad \gamma = \sqrt{2}u$$

$$\lim_{u \rightarrow 0} Z_{W_\delta}^*(u) = 1, \quad \lim_{u \rightarrow \infty} \sqrt{i}u Z_{W_\delta}^*(u) = 1$$

$$\text{Re } Z_{W_\delta}^*(\gamma) = \frac{\sin(\gamma) + \sinh(\gamma)}{\gamma (\cos(\gamma) + \cosh(\gamma))}, \quad \text{Im } Z_{W_\delta}^*(\gamma) = \frac{\sin(\gamma) - \sinh(\gamma)}{\gamma (\cos(\gamma) + \cosh(\gamma))}$$

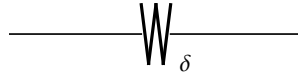


Figure 1.8: Bounded diffusion impedance.

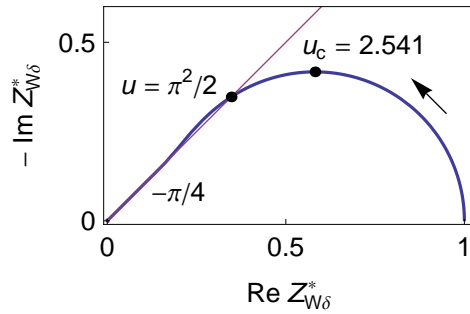


Figure 1.9: Nyquist diagram of the reduced bounded diffusion impedance. ( $u = \pi^2/2$  [40]).

### 1.3.1 Randles circuit

Fig. 1.10.

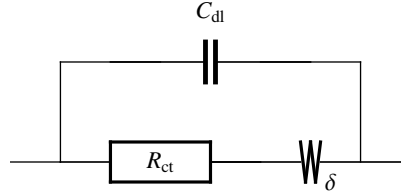


Figure 1.10: Randles circuit for bounded diffusion.

#### Impedance

$$Z_f(u) = R_{ct} + R_d \frac{\tanh \sqrt{i} u}{\sqrt{i} u}, \quad u = \tau_d \omega, \quad \tau_d = \delta^2 / D$$

$$\operatorname{Re} Z_f(\gamma) = R_{ct} + R_d \frac{\sin(\gamma) + \sinh(\gamma)}{\gamma (\cos(\gamma) + \cosh(\gamma))}, \quad \gamma = \sqrt{2} u$$

$$\operatorname{Im} Z_f(\gamma) = R_d \frac{\sin(\gamma) - \sinh(\gamma)}{\gamma (\cos(\gamma) + \cosh(\gamma))}$$

$$Z(u) = \frac{Z_f(u)}{1 + i(u/\tau_d) C_{dl} Z_f(u)} = \frac{R_{ct} + R_d \frac{\tanh \sqrt{i} u}{\sqrt{i} u}}{1 + i(u/\tau_d) C_{dl} \left( R_{ct} + R_d \frac{\tanh \sqrt{i} u}{\sqrt{i} u} \right)}$$

#### Reduced impedance

$$Z^*(u) = \frac{Z(u)}{R_{ct} + R_d} = \frac{1}{(1 + \rho) \left( \frac{i T u}{\rho} + \frac{1}{\rho + \frac{\tanh \sqrt{i} u}{\sqrt{i} u}} \right)}$$

$$\rho = R_{ct}/R_d, \quad T = \tau_f/\tau_d, \quad \tau_f = R_{ct} C_{dl}$$

Fig. 1.11

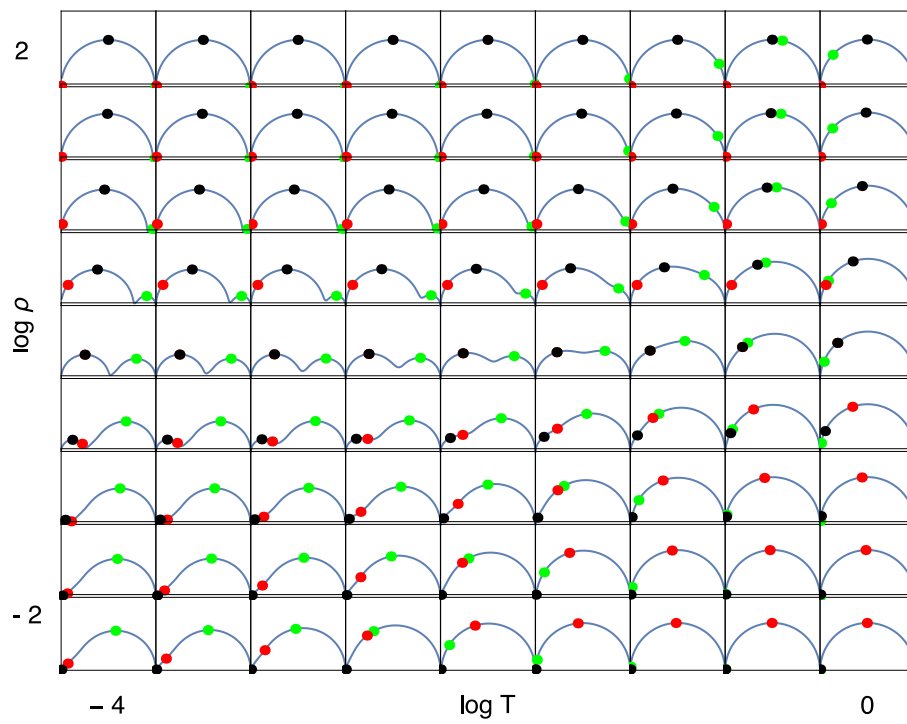


Figure 1.11: Impedance diagram array for the Randles circuit with bounded diffusion (Fig. 1.10). Green points:  $u_{c1} = 2.54$ , red points:  $u_{c2} = \rho/T$ , black points:  $u_{c3} = 1/T$ .

### 1.3.2 Corrosion equivalent circuit

Corrosion of a metal M with limitation by mass transport of oxidant (Fig. 1.12) on a rotating disk electrode (RDE) [34].

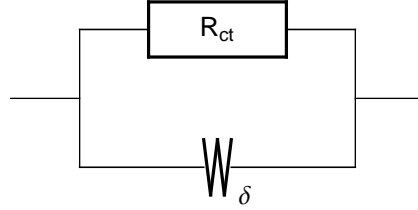


Figure 1.12: Equivalent circuit for corrosion of a metal M with limitation by mass transport of oxidant.  $R_{ct}$  : charge transfer of the reaction of metal oxidation.

$$Z(u) = \frac{R_{ct} R_d \frac{\tanh \sqrt{i u}}{\sqrt{i u}}}{R_{ct} + R_d \frac{\tanh \sqrt{i u}}{\sqrt{i u}}}, \quad u = \tau_d \omega, \quad \tau_d = \delta^2 / D \quad (1.1)$$

$$Z^*(u) = (1 + \alpha) \frac{Z(u)}{R_d} = (1 + \alpha) \frac{\frac{\tanh \sqrt{i u}}{\sqrt{i u}}}{1 + \alpha \frac{\tanh \sqrt{i u}}{\sqrt{i u}}}, \quad \alpha = \frac{R_d}{R_{ct}} \quad (1.2)$$

Two limiting cases (Fig. 1.13):

- $\alpha \ll 1$ :

$$Z^*(u) \approx \frac{\tanh \sqrt{i u}}{\sqrt{i u}}, \quad u_{c1} = 2.541, \quad \text{quarter of lemniscate, (Fig. 1.8)} \quad (1.3)$$

- $\alpha \gg 1$ :

$$Z^*(u) \approx \frac{\alpha}{\alpha + \sqrt{i u}}, \quad u_{c2} = \alpha^2, \quad \text{quarter of circle, (Fig. 1.7)} \quad (1.4)$$

## 1.4 Analytical approximation

### 1.4.1 Analytical approximation #1

[13], Fig. 1.14.

$$Z^*(u) = \frac{\sqrt{\gamma + i u}}{\sqrt{\gamma}(1 + i u)}, \quad \gamma = 1.877 \quad (1.5)$$

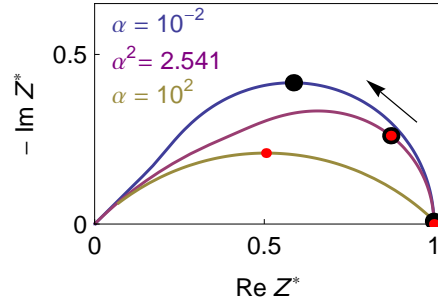


Figure 1.13: Nyquist diagram of the corrosion equivalent circuit. Large black dot :  $u_{c1} = 2.541$ , small red dot :  $u_{c2} = \alpha^2$ .

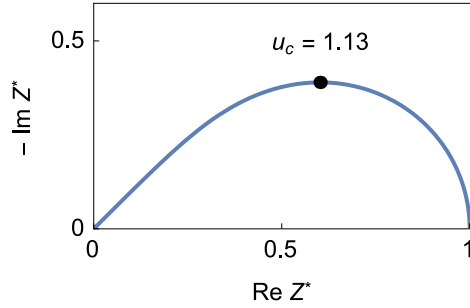


Figure 1.14: Nyquist diagram of the analytical approximation #1 (Eq. (1.5)).

### 1.4.2 Analytical approximation #2

[30], Fig. 1.15.

$$Z^*(f) = \frac{Z(f)}{R_d} = \frac{\sqrt{\gamma^2 + \tau_d i 2\pi f}}{\gamma + \tau_d i 2\pi f}, \quad \tau_d = \frac{\delta_d^2}{D} \quad (1.6)$$

where  $\gamma$  and  $\tau_d$  depend on the Schmidt number  $Sc$ . For  $Sc \in [10^2, 10^5]$ :

$$\gamma = \frac{1.9930 - 1.6319 Sc^{-1/3}}{1 - 0.7248 Sc^{-1/3}} \quad (1.7)$$

$$\tau_d = \frac{1.61173^2}{\Omega} Sc^{1/3} (1 + 0.2980 Sc^{-1/3} + 0.14514 Sc^{-2/3} + 0.07020 Sc^{-1})^2 \quad (1.8)$$

## 1.5 Radial cylindrical diffusion

$d = 2$  [19] (Fig. 1.1)

### 1.5.1 Finite-length diffusion outside a cylinder

$$Z^*(u) = \frac{I_0(\sqrt{i u} \rho) K_0(\sqrt{i u}) - I_0(\sqrt{i u}) K_0(\sqrt{i u} \rho)}{\text{Log}(\rho) \sqrt{i u} \left( I_1(\sqrt{i u}) K_0(\sqrt{i u} \rho) + I_0(\sqrt{i u} \rho) K_1(\sqrt{i u}) \right)}$$

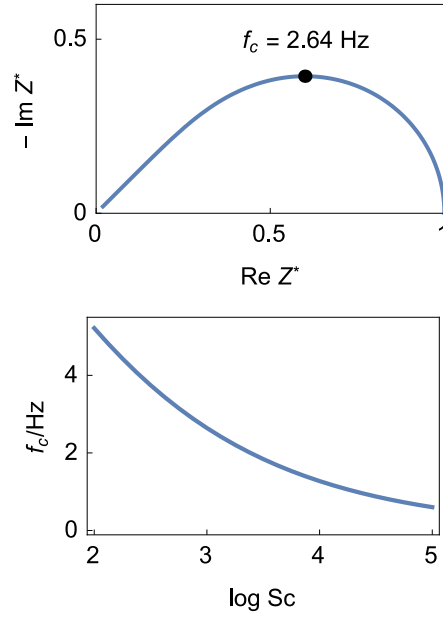


Figure 1.15: Nyquist diagram of the analytical approximation #2 (Eqs. (1.6)-(1.8),  $Sc = 10^3$ ,  $\Omega = 2000 \text{ tr min}^{-1}$ ) and change of  $f_c$  with  $Sc$ .

$$u = r_0^2 \omega / D, \quad \rho = r_\delta / r_0$$

Fig. 1.16 rectifies erroneous Figs. 7 and 8 in [31].

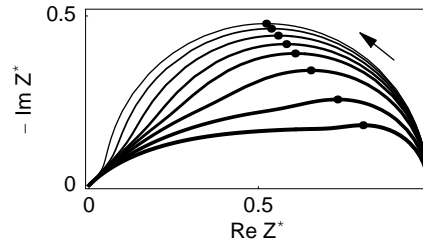


Figure 1.16: Central ( $\rho < 1$ ) and outside ( $\rho > 1$ ) cylindrical diffusion impedance.  $\rho = r_\delta / r_0 = 10^{-2}, 10^{-1}, 0.4, 1.01, 2, 5, 20, 100$ . The thickness increases with  $\rho$ . Dots: reduced characteristic angular frequency (apex of the impedance arc):  $u_c = 0.514484, 1.22194, 4.74992, 25516., 3.40142, 0.298271, 0.0186746, 0.000800438$ .

### 1.5.2 Semi-infinite outside a cylinder

$$\lim_{\rho \rightarrow \infty} Z^*(u) = \frac{K_0(\sqrt{i}u)}{\sqrt{i}u K_1(\sqrt{i}u)}$$

(Fig. 1.6)

## 1.6 Spherical diffusion

$d = 3$  [19] (Fig. 1.1)

### 1.6.1 Finite-length diffusion outside a sphere, reduced impedance # 1

(Fig. 1.17)

$$Z^*(u) = \frac{1}{(1 - 1/\rho) \left(1 + \sqrt{i u} \coth(\sqrt{i u} (-1 + \rho))\right)}, \quad u = r_0^2 \omega / D, \quad \rho = r_\delta / r_0$$

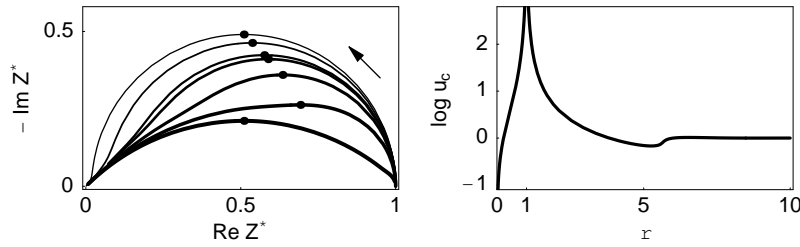


Figure 1.17: Central ( $\rho < 1$ ) and outside ( $\rho > 1$ ) spherical diffusion impedance.  $\rho = r_\delta / r_0 = 0.1, 0.4, 0.91, 1.1, 2, 5, 50$ . Line thickness increases with  $\rho$ . Dots: reduced characteristic angular frequency:  $u_c = r_0^2 \omega / D = 0.3632, 3.095, 289, 275.8, 4.547, 0.6927, 1$ . Change of  $\log u_c$  with  $\rho$ .

### 1.6.2 Finite outside sphere, reduced impedance # 2

(Fig. 1.18)

$$Z^*(u) = \frac{1 + \delta}{\delta + \sqrt{i u} \coth(\sqrt{i u})}, \quad u = (r_\delta - r_0)^2 \omega / D, \quad \delta = (r_\delta - r_0) / r_0$$

### 1.6.3 Infinite outside sphere

(Fig. 1.7)

$$\lim_{\rho \rightarrow \infty} Z^*(u) = \frac{1}{1 + \sqrt{i u}}, \quad u = r_0^2 \omega / D$$

$$\text{Re } Z^*(u) = \frac{2 + \sqrt{2u}}{2(1 + \sqrt{2u})}, \quad \text{Im } Z^*(u) = -\frac{\sqrt{u}}{\sqrt{2}(1 + \sqrt{2u} + u)}$$



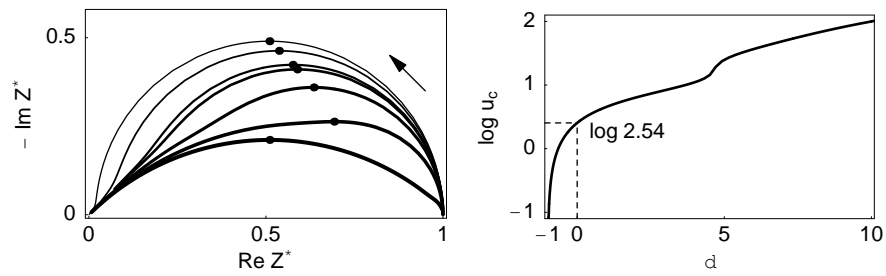


Figure 1.18: Central ( $\delta < 0$ ) and outside ( $\delta > 0$ ) spherical diffusion impedance.  $\delta = (r_\delta - r_0)/r_0 = -0.99, -0.8, -0.5, -0.1, 0.1, 1, 3, 100$ . Line thickness increases with  $\delta$ . Dots: reduced characteristic angular frequency:  $u_c = (r_\delta - r_0)^2 \omega / D = 0.0299, 0.577, 1.37, 2.32, 2.76, 4.55, 8.33, 10^4$ ,  $u_c$  increases with  $\delta$ . Change of  $\log u_c$  with  $\delta$ .

## Chapter 2

# Mass transfer by diffusion, restricted diffusion

### 2.1 General diffusion equations

From:

$$\frac{\partial \Delta c(x,t)}{\partial t} = D x^{1-d} \frac{\partial}{\partial x} \left( x^{d-1} \frac{\partial \Delta c(x,t)}{\partial x} \right)$$

where  $\Delta$  denotes a small deviation (or excursion) from the initial steady-state value,  $d = 1$  corresponds to a planar electrode,  $d = 2$  to a cylindrical electrode (radial diffusion) and  $d = 3$  to a spherical electrode [5, 33] (Fig. 1.1), it is obtained, using the condition  $\Delta J(r_\delta) = 0$ :

$$Z^*(u) \propto \frac{\Delta c(r_0, i u)}{\Delta J(r_0, i u)} = \frac{I_{d/2-1}(\sqrt{i u}) K_{d/2}(\sqrt{i u} \rho) + I_{d/2}(\sqrt{i u} \rho) K_{d/2-1}(\sqrt{i u})}{\sqrt{i u} (I_{d/2}(\sqrt{i u} \rho) K_{d/2}(\sqrt{i u}) - I_{d/2}(\sqrt{i u}) K_{d/2}(\sqrt{i u} \rho))}$$

Terminology [32]: bounded system [20], finite-space diffusion [1, 2], finite length diffusion [23], restricted diffusion [11, 10, 14], reflective boundary condition [36], impermeable boundary [49], impermeable barrier condition [19], impermeable surface [12].



Figure 2.1: Restricted diffusion impedance.  $d = 1$ : thin planar layer,  $d = 2$ : cylinder,  $d = 3$ : sphere.

Internal cylinder and sphere with null radius,  $r_0 = 0$ .

$$Z^*(u) = \frac{I_{d/2-1}(\sqrt{i u})}{\sqrt{i u} I_{d/2}(\sqrt{i u})}$$

Fig. 2.2.

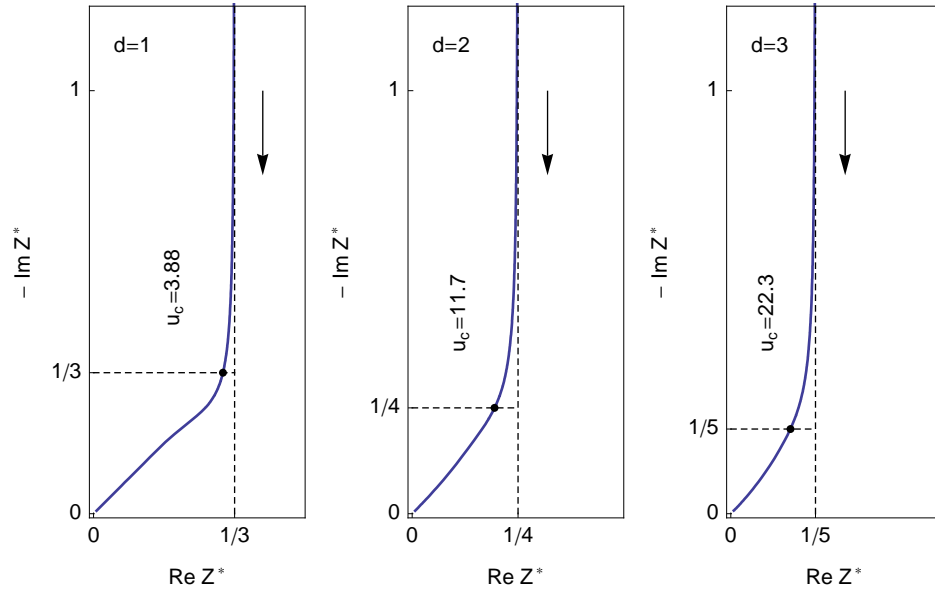


Figure 2.2: Nyquist diagram of the reduced impedance for the restricted diffusion impedance  $Z^*(u)$  plotted for  $d = 1, 2, 3$ .  $d = 1$ : thin planar layer,  $d = 2$ : cylinder,  $d = 3$ : sphere. Dots: reduced characteristic angular frequency:  $u_{c1} = 3.88$ ,  $u_{c2} = 11.7$ ,  $u_{c3} = 22.3$ .

### Low frequency limit

Fig. 2.3.

$$u \rightarrow 0 \Rightarrow Z^*(u) \approx \frac{1}{d+2} - \frac{id}{u}$$

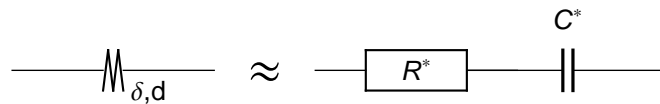


Figure 2.3: Low frequency equivalent circuit for restricted diffusion impedance.  $R^* = 1/(d+2)$ ,  $C^* = 1/d$ .

### High frequency limit

Fig. 2.4.

$$u \rightarrow \infty \Rightarrow Z^*(u) \approx \frac{1}{\sqrt{iu}}, \quad \lim_{u \rightarrow \infty} \sqrt{iu} Z^*(u) = 1$$



Figure 2.4: High frequency equivalent circuit for restricted diffusion impedance.

## 2.2 Linear diffusion and modified linear diffusion

### 2.2.1 Linear diffusion

$d = 1$

$$Z^*(u) = \frac{I_{d/2-1}(\sqrt{i}u)}{\sqrt{i}u I_{d/2}(\sqrt{i}u)} = \frac{I_{-1/2}(\sqrt{i}u)}{\sqrt{i}u I_{1/2}(\sqrt{i}u)} = \frac{\coth \sqrt{i}u}{\sqrt{i}u}$$

Reduced characteristic angular frequency:  $u_{c1} \approx 3 (d(d+2))$  [5], 5.12 [3], 4 [8], 3.88 [7].

$$\lim_{u \rightarrow 0} Z^*(u) = \frac{1}{3} + \frac{1}{i u}, \quad \lim_{u \rightarrow \infty} \sqrt{i}u Z^*(u) = 1$$

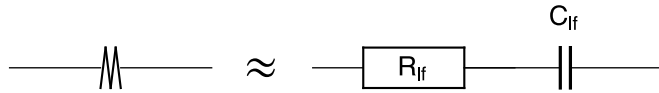
$$u = \tau_d \omega, \quad \tau_d = \delta^2 / D, \quad \gamma = \sqrt{2u}$$

$$\operatorname{Re} Z^*(\gamma) = \frac{\sin(\gamma) - \sinh(\gamma)}{\gamma (\cos(\gamma) - \cosh(\gamma))}; \quad \operatorname{Im} Z^*(\gamma) = \frac{\sin(\gamma) + \sinh(\gamma)}{\gamma (\cos(\gamma) - \cosh(\gamma))}$$

#### Low frequency limit

Equivalent circuit: Fig. 2.5 (<sup>1</sup>).

$$Z^*(u) = \frac{Z(u)}{R_d} \Rightarrow \lim_{\omega \rightarrow 0} Z(\omega) = \frac{R_d}{3} + \frac{R_d}{\tau_d i \omega} = R_{lf} + \frac{1}{C_{lf} i \omega}, \quad R_{lf} = \frac{R_d}{3}, \quad C_{lf} = \frac{\tau_d}{R_d}$$

Figure 2.5: Low frequency equivalent circuit for restricted diffusion impedance.  $R_{lf} = R_d/3$ ,  $C_{lf} = \tau_d/R_d$ .

#### Randles circuit for restricted linear diffusion

**Randles circuit** Fig. 2.6.

<sup>1</sup> For unit problems, don't forget the Farad unit :  $F = s/\Omega$ .

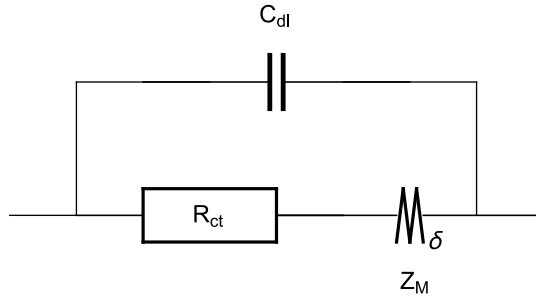


Figure 2.6: Randles circuit for restricted diffusion.

### Impedance

$$Z_f(u) = R_{ct} + R_d \frac{\coth \sqrt{i} u}{\sqrt{i} u}, \quad Z(u) = \frac{Z_f(u)}{1 + i(u/\tau_d) C_{dl} Z_f(u)}, \quad u = \tau_d \omega, \quad \tau_d = \delta^2/D$$

### Reduced impedance [9]

$$Z(u) = \frac{3(1 + T/\rho)^2}{(1 + 3\rho) \left( \frac{iTu}{\rho} + \frac{1}{\rho + \frac{\coth(\sqrt{i}u)}{\sqrt{i}u}} \right)}$$

$$\rho = R_{ct}/R_d, \quad T = \tau_f/\tau_d, \quad \tau_f = R_{ct} C_{dl}$$

## 2.2.2 Modified restricted diffusion impedance

$\sqrt{i}u$  replaced by  $(iu)^{\frac{\alpha}{2}}$  ( $\alpha$ : dispersion parameter) [8, 7, 39], Fig. 2.8.

$$Z^*(u) = \frac{\coth(iu)^{\frac{\alpha}{2}}}{(iu)^{\frac{\alpha}{2}}}, \quad u = \tau_d \omega, \quad \tau_d = \delta^2/D$$

$$\text{Re } Z^*(u) = \frac{u^{-\alpha/2} (\sin(\frac{\pi\alpha}{4}) \sin(2u^{\alpha/2} \sin(\frac{\pi\alpha}{4})) - \cos(\frac{\pi\alpha}{4}) \sinh(2u^{\alpha/2} \cos(\frac{\pi\alpha}{4})))}{\cos(2u^{\alpha/2} \sin(\frac{\pi\alpha}{4})) - \cosh(2u^{\alpha/2} \cos(\frac{\pi\alpha}{4}))}$$

$$\text{Im } Z^*(u) = \frac{u^{-\alpha/2} (\cos(\frac{\pi\alpha}{4}) \sin(2u^{\alpha/2} \sin(\frac{\pi\alpha}{4})) + \sin(\frac{\pi\alpha}{4}) \sinh(2u^{\alpha/2} \cos(\frac{\pi\alpha}{4})))}{\cos(2u^{\alpha/2} \sin(\frac{\pi\alpha}{4})) - \cosh(2u^{\alpha/2} \cos(\frac{\pi\alpha}{4}))}$$

### Low frequency limit

Equivalent circuit: Fig. 2.9.

$$u \rightarrow 0 \Rightarrow Z^*(u) \approx \frac{1}{3} + \frac{1}{(iu)^\alpha}$$

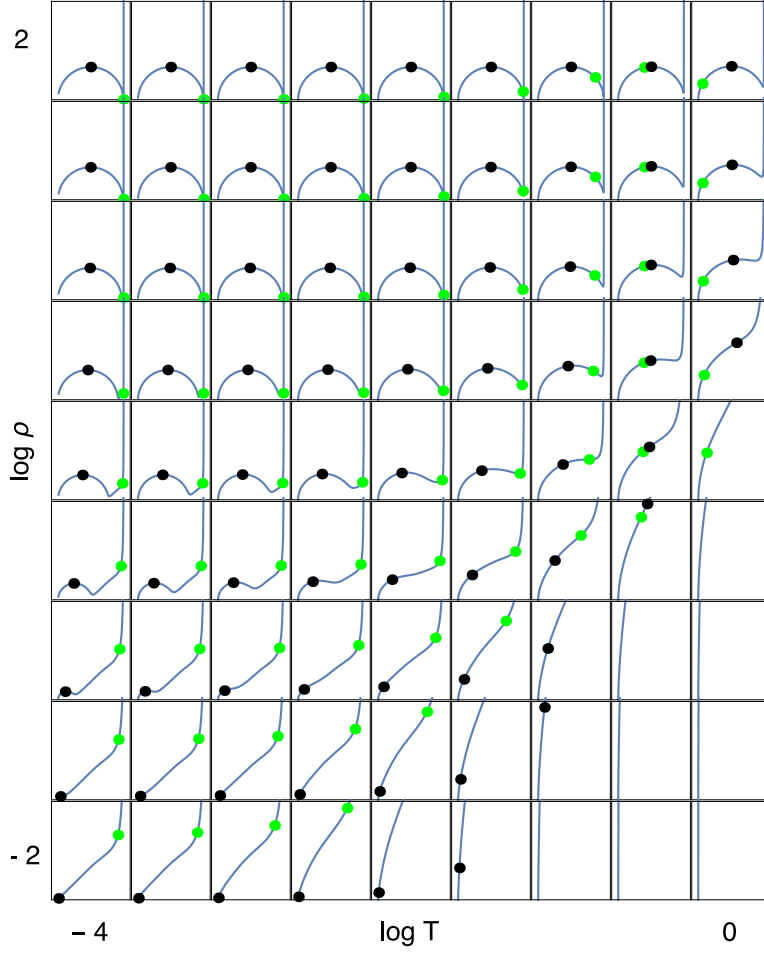


Figure 2.7: Impedance diagram array for the Randles circuit with restricted diffusion (Fig. 2.6). Green points:  $u_{c1} = 3.88$ , black points:  $u_{c2} = 1/T$ .

$$Z^*(u) = \frac{Z(u)}{R_d} \Rightarrow \lim_{\omega \rightarrow 0} Z(\omega) = \frac{R_d}{3} + \frac{R_d}{(i\tau_d \omega)^\alpha} = R_{lf} + \frac{1}{Q_{lf}(i\omega)^\alpha}, \quad R_{lf} = \frac{R_d}{3}, \quad Q_{lf} = \frac{\tau_d^\alpha}{R_d}$$

### 2.2.3 Anomalous diffusion impedance

[6], Fig. 2.10.

$$Z(\omega) = R_d \frac{\coth(i\omega \tau_d)^{\gamma/2}}{(i\omega \tau_d)^{1-\gamma/2}}, \quad \gamma \leq 1$$

$$Z(u)^* = \frac{Z(\omega)}{R_d} = \frac{\coth(iu)^{\gamma/2}}{(iu)^{1-\gamma/2}}, \quad u = \omega \tau_d, \tau_d = \left(\frac{\delta^2}{D}\right)^{1/\gamma}$$

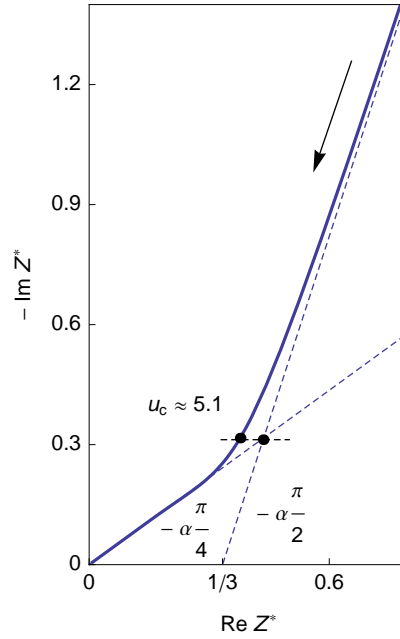


Figure 2.8: Nyquist diagram of the reduced modified restricted diffusion impedance, plotted for  $\alpha = 0.8$ .  $u_c$  depends on  $\alpha$  [7].

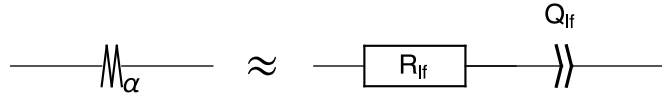


Figure 2.9: Low frequency equivalent circuit for modified restricted diffusion impedance.  $R_{lf} = R_d/3$ ,  $Q_{lf} = \tau_d^\alpha/R_d$ .  $Q_{lf}$  unit :  $\frac{s^\alpha}{\Omega} = \frac{s}{\Omega} \frac{s^\alpha}{s} = F s^{\alpha-1}$ .

The  $D$  unit ( $D/\text{cm}^2 \text{ s}^{-\gamma}$ ) depends on  $\gamma$ .

$$\text{Re } Z^*(u) = \frac{u^{\frac{\gamma}{2}-1} \left( \cos\left(\frac{\pi\gamma}{4}\right) \sin\left(2u^{\gamma/2} \sin\left(\frac{\pi\gamma}{4}\right)\right) - \sin\left(\frac{\pi\gamma}{4}\right) \sinh\left(2u^{\gamma/2} \cos\left(\frac{\pi\gamma}{4}\right)\right) \right)}{\cos\left(2u^{\gamma/2} \sin\left(\frac{\pi\gamma}{4}\right)\right) - \cosh\left(2u^{\gamma/2} \cos\left(\frac{\pi\gamma}{4}\right)\right)}$$

$$\text{Im } Z^*(u) = \frac{u^{\frac{\gamma}{2}-1} \left( \sin\left(\frac{\pi\gamma}{4}\right) \sin\left(2u^{\gamma/2} \sin\left(\frac{\pi\gamma}{4}\right)\right) + \cos\left(\frac{\pi\gamma}{4}\right) \sinh\left(2u^{\gamma/2} \cos\left(\frac{\pi\gamma}{4}\right)\right) \right)}{\cos\left(2u^{\gamma/2} \sin\left(\frac{\pi\gamma}{4}\right)\right) - \cosh\left(2u^{\gamma/2} \cos\left(\frac{\pi\gamma}{4}\right)\right)}$$

## 2.3 Cylindrical diffusion

$d = 2$ ,  $\delta$ : cylinder radius

$$Z^*(u) = \frac{I_{d/2-1}(\sqrt{i}u)}{\sqrt{i}u I_{d/2}(\sqrt{i}u)} = \frac{I_0(\sqrt{i}u)}{\sqrt{i}u I_1(\sqrt{i}u)}$$

$$\lim_{u \rightarrow 0} Z^*(u) = \frac{1}{4} - \frac{2i}{u}, \quad \lim_{u \rightarrow \infty} \sqrt{i}u Z^*(u) = 1$$

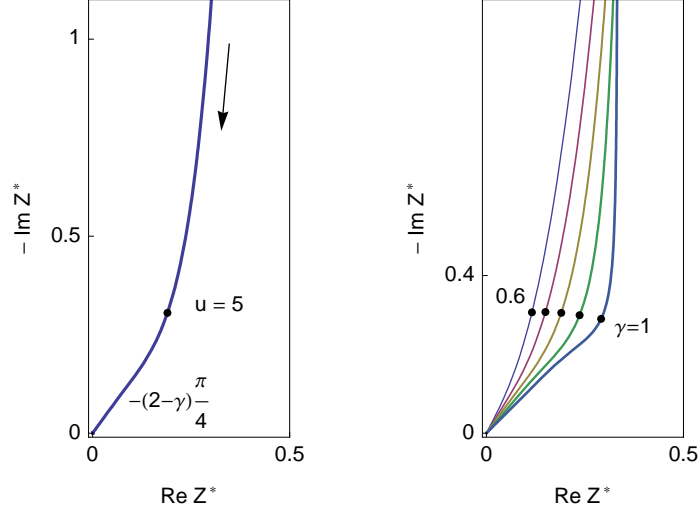


Figure 2.10: Nyquist diagram of the reduced anomalous diffusion impedance. Left:  $\gamma = 0.8$ , right: change of Nyquist diagram with  $\gamma$  ( $\gamma : 1, 0.9, 0.8, 0.7, 0.6$ ). Dots:  $u = 5$  [6].

$$u = \tau_d \omega, \quad \tau_d = \delta^2/D$$

### Low frequency limit

Equivalent circuit:  $R_{lf} + C_{lf}$ .

$$Z^*(u) = \frac{Z(u)}{R_d} \Rightarrow \lim_{\omega \rightarrow 0} Z(\omega) = \frac{R_d}{4} + \frac{2R_d}{\tau_d i \omega} = R_{lf} + \frac{1}{C_{lf} i \omega}, \quad R_{lf} = \frac{R_d}{4}, \quad C_{lf} = \frac{\tau_d}{2R_d}$$

## 2.4 Spherical diffusion

$d = 3$ ,  $\delta$ : sphere radius

$$Z^*(u) = \frac{I_{d/2-1}(\sqrt{i u})}{\sqrt{i u} I_{d/2}(\sqrt{i u})} = \frac{I_{1/2}(\sqrt{i u})}{\sqrt{i u} I_{3/2}(\sqrt{i u})} = \frac{1}{-1 + \sqrt{i u} \coth \sqrt{i u}}$$

$$\lim_{u \rightarrow 0} Z^*(u) = \frac{1}{5} - \frac{3i}{u}, \quad \lim_{u \rightarrow \infty} \sqrt{i u} Z^*(u) = 1$$

$$u = \tau_d \omega, \quad \tau_d = \delta^2/D, \quad \gamma = \sqrt{2u}$$

$$\operatorname{Re} Z^*(\gamma) = \frac{2 \cos(\gamma) - 2 \cosh(\gamma) + \gamma \sin(\gamma) + \gamma \sinh(\gamma)}{(-2 + \gamma^2) \cos(\gamma) + (2 + \gamma^2) \cosh(\gamma) - 2\gamma (\sin(\gamma) + \sinh(\gamma))}$$

$$\operatorname{Im} Z^*(\gamma) = \frac{\gamma (\sin(\gamma) - \sinh(\gamma))}{(-2 + \gamma^2) \cos(\gamma) + (2 + \gamma^2) \cosh(\gamma) - 2\gamma (\sin(\gamma) + \sinh(\gamma))}$$



**Low frequency limit**Equivalent circuit:  $R_{lf} + C_{lf}$ .

$$Z^*(u) = \frac{Z(u)}{R_d} \Rightarrow \lim_{\omega \rightarrow 0} Z(\omega) = \frac{R_d}{5} + \frac{3R_d}{\tau_d i \omega} = R_{lf} + \frac{1}{C_{lf} i \omega}, \quad R_{lf} = \frac{R_d}{5}, \quad C_{lf} = \frac{\tau_d}{3R_d}$$

## Chapter 3

# Gerischer and diffusion-reaction impedance

### 3.1 Gerischer and modified Gerischer impedance

#### 3.1.1 Gerischer impedance

$$Z_G^*(u) = \frac{1}{\sqrt{1+iu}} \quad (3.1)$$

"In view of the earliest derivation of such an impedance by Gerischer, [16] it seems a good idea to name it the "Gerischer impedance"  $Z_G$ " [43, 45].

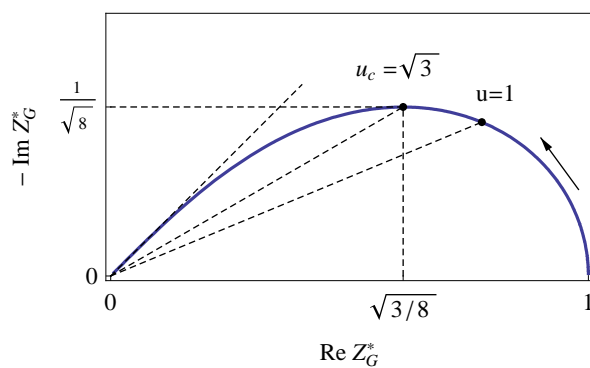


Figure 3.1: Reduced Gerischer impedance. Some characteristic values are given in [24, 25]. Phase angle for dashed lines :  $-\pi/8$ ,  $-\pi/6$  and  $-\pi/4$  respectively.

$$\lim_{u \rightarrow 0} Z_G^*(u) = 1, \quad \lim_{u \rightarrow \infty} \sqrt{iu} Z_G^*(u) = 1$$

$$\operatorname{Re} Z_G^*(u) = \frac{\cos\left(\frac{\arctan(u)}{2}\right)}{(1+u^2)^{1/4}} = \frac{\sqrt{\sqrt{1+u^{-2}}+u^{-1}}}{\sqrt{2}\sqrt{1+u^{-2}}\sqrt{u}}$$

$$\operatorname{Im} Z_G^*(u) = -\frac{\sin\left(\frac{\arctan(u)}{2}\right)}{(1+u^2)^{1/4}} = -\frac{\sqrt{\sqrt{1+u^{-2}}-u^{-1}}}{\sqrt{2}\sqrt{1+u^{-2}}\sqrt{u}}$$

$$\frac{d\operatorname{Im} Z_G^*(u)}{du} = \frac{-2 + \sqrt{1+u^{-2}}u}{2\sqrt{2}\sqrt{1+u^{-2}}\sqrt{\sqrt{1+u^{-2}}-\frac{1}{u}}\sqrt{u}(1+u^2)} = 0 \Rightarrow u_c = \sqrt{3}$$

$$\text{Diagnostic criterion [17, 35] } \operatorname{Re} Y_G^*(u)^2 - \operatorname{Im} Y_G^*(u)^2 = 1$$

### 3.1.2 Modified Gerischer impedance #1

$$Z_{G\alpha}^*(u) = \frac{1}{\sqrt{1+(iu)^\alpha}}$$

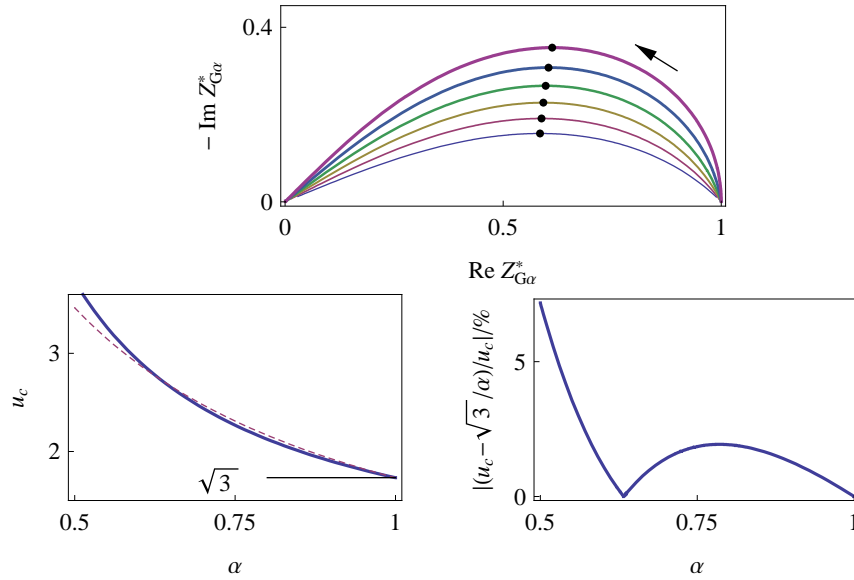


Figure 3.2: Reduced modified Gerischer impedance.  $\alpha = 0.5, 0.6, 0.7, 0.8, 0.9, 1$ . Line thickness increases with  $\alpha$ . Dots: characteristic frequency  $u_c$  at the apex of the impedance arc. Change of  $u_c$  for the modified Gerischer impedance (solid line) and change of  $\sqrt{3}/\alpha$  with  $\alpha$  (dashed line).  $u_c \approx \sqrt{3}/\alpha$  for  $\alpha \in [0.53, 1]$  ( $|(u_c - \sqrt{3}/\alpha)|/u_c < 5\%$ ).

$$\operatorname{Re} Z_{G\alpha}^*(u) = \frac{\cos\left(\frac{1}{2}\arctan\left(\frac{u^\alpha \sin\left(\frac{\pi\alpha}{2}\right)}{1 + u^\alpha \cos\left(\frac{\pi\alpha}{2}\right)}\right)\right)}{\left(1 + u^{2\alpha} + 2u^\alpha \cos\left(\frac{\pi\alpha}{2}\right)\right)^{\frac{1}{4}}}$$

$$\operatorname{Im} Z_{G\alpha}^*(u) = -\frac{\sin\left(\frac{1}{2}\arctan\left(\frac{u^\alpha \sin\left(\frac{\pi\alpha}{2}\right)}{1 + u^\alpha \cos\left(\frac{\pi\alpha}{2}\right)}\right)\right)}{\left(1 + u^{2\alpha} + 2u^\alpha \cos\left(\frac{\pi\alpha}{2}\right)\right)^{\frac{1}{4}}}$$

### 3.1.3 Modified Gerischer impedance #2

$$Z_{G\alpha 2}^*(u) = \frac{1}{(1 + iu)^{\alpha/2}}, \quad \alpha \in [0, 1]$$

$$\operatorname{Re} Z_{G\alpha 2}^*(u) = (u^2 + 1)^{-\alpha/4} \cos\left(\frac{1}{2}\alpha \arctan(u)\right)$$

$$\operatorname{Im} Z_{G\alpha 2}^*(u) = - (u^2 + 1)^{-\alpha/4} \sin\left(\frac{1}{2}\alpha \arctan(u)\right)$$

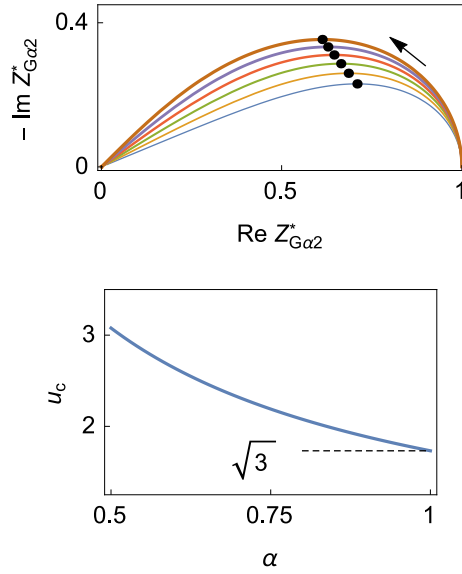


Figure 3.3: Reduced modified Gerischer impedance #2.  $\alpha = 0.5, 0.6, 0.7, 0.8, 0.9, 1$  ( $\alpha = 1$ : Gerischer impedance Eq. (3.1)). Line thickness increases with  $\alpha$ . Dots: characteristic frequency  $u_c$  at the apex of the impedance arc. Change of  $u_c$  for the modified Gerischer impedance #2.

### 3.1.4 Modified Gerischer impedance #3

[37, 27], Fig. 3.4.

$$Z_{G\alpha 3}^*(u) = \frac{1}{(1 + iu)^\alpha}, \quad \alpha \in [0, 1]$$

$$\operatorname{Re} Z_{G\alpha 3}^*(u) = (u^2 + 1)^{-\alpha/2} \cos(\alpha \arctan(u))$$

$$\operatorname{Im} Z_{G\alpha 3}^*(u) = - (u^2 + 1)^{-\alpha/2} \sin(\alpha \arctan(u))$$

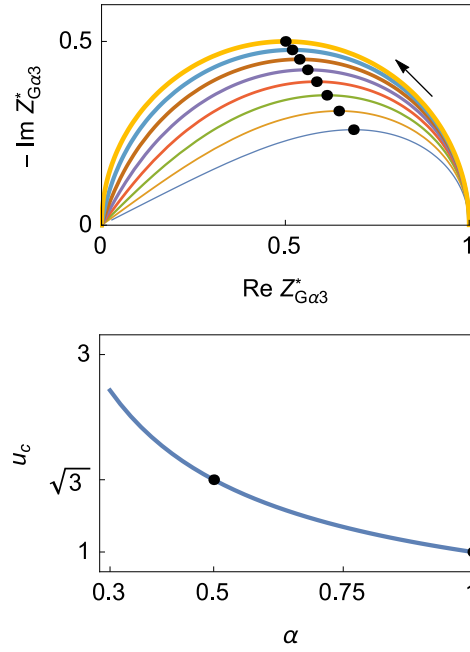


Figure 3.4: Reduced modified Gerischer impedance #3.  $\alpha = 0.3, 0.4, 0.5, 0.6, 0.7, 0.8, 0.9, 1$  ( $\alpha = 0.5$ : Gerischer impedance Eq. (3.1)). Line thickness increases with  $\alpha$ . Dots: characteristic frequency  $u_c$  at the apex of the impedance arc. Change of  $u_c$  for the modified Gerischer impedance #3.

### 3.1.5 Havriliak-Negami impedance

[18, 21], Fig. 3.5.

$$Z_{\text{HN}}^*(u) = \frac{1}{(1 + (iu)^\alpha)^\beta} \quad (3.2)$$

$$\text{Re } Z_{\text{HN}}^*(u) = \left( u^{2\alpha} + 2 \cos\left(\frac{\pi\alpha}{2}\right) u^\alpha + 1 \right)^{-\beta/2} \cos\left( \beta \arctan\left( \frac{\sin\left(\frac{\pi\alpha}{2}\right) u^\alpha}{\cos\left(\frac{\pi\alpha}{2}\right) u^\alpha + 1} \right) \right) \quad (3.3)$$

$$\text{Im } Z_{\text{HN}}^*(u) = - \left( u^{2\alpha} + 2 \cos\left(\frac{\pi\alpha}{2}\right) u^\alpha + 1 \right)^{-\beta/2} \sin\left( \beta \arctan\left( \frac{\sin\left(\frac{\pi\alpha}{2}\right) u^\alpha}{\cos\left(\frac{\pi\alpha}{2}\right) u^\alpha + 1} \right) \right) \quad (3.4)$$

- $\beta = 1/2 \Rightarrow$  modified Gerischer impedance #1 (cf. § 3.1.2, p. 26)
- $\alpha = 1 \Rightarrow$  modified Gerischer impedance #2, (cf. § 3.1.3, p. 27), #3, (cf. § 3.1.4, p. 27)

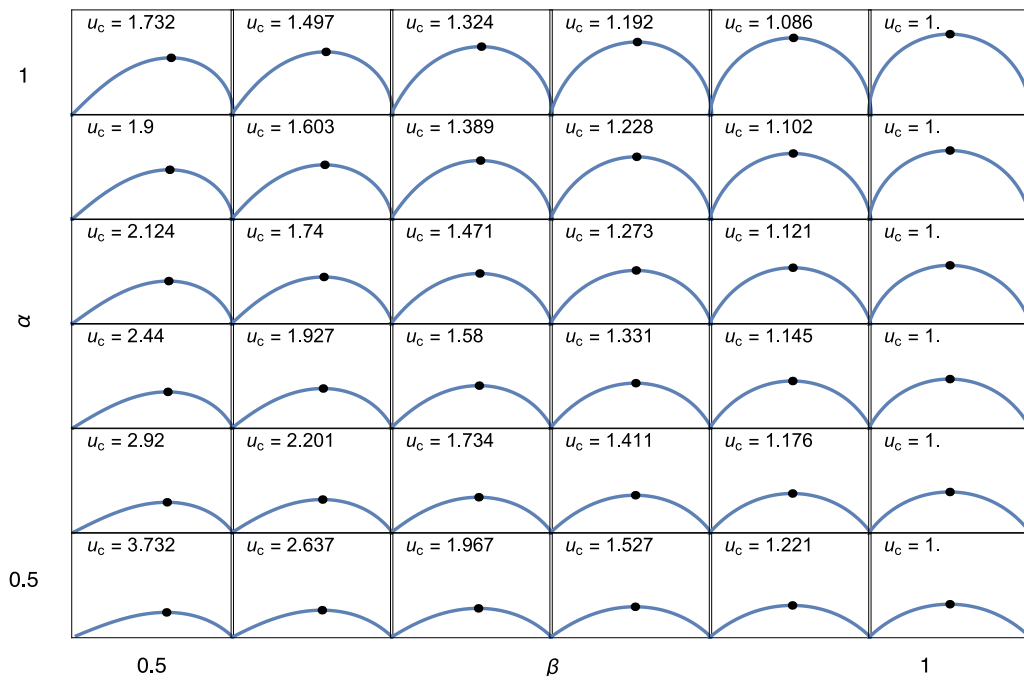


Figure 3.5: Impedance diagram array for the reduced Havriliak-Negami impedance.  $u_c = \sqrt{3}$  ( $\alpha = 1, \beta = 1/2$ ),  $u_c = 2 + \sqrt{3}$  ( $\alpha = \beta = 1/2$ ),  $u_c = 1$  ( $\beta = 1, \forall \alpha$ ).

## 3.2 Diffusion-reaction impedance

### 3.2.1 Reduced impedance #1

$$Z^*(u) = \frac{\sqrt{\lambda}}{\tanh \sqrt{\lambda}} \frac{\tanh \sqrt{i u + \lambda}}{\sqrt{i u + \lambda}}$$

$$\lim_{u \rightarrow 0} Z^*(u) = 1, \quad \lim_{u \rightarrow \infty} \sqrt{i u + \lambda} Z^*(u) = \sqrt{\lambda} \coth \sqrt{\lambda}$$

$$\lambda \rightarrow 0 \Rightarrow Z^*(u) \approx Z_{W\delta}^*(u) = \frac{\tanh \sqrt{i u}}{\sqrt{i u}}, \quad \lambda \rightarrow \infty \Rightarrow Z^*(u) \approx Z_G^*(u/\lambda) = \frac{1}{\sqrt{1 + i u/\lambda}}$$

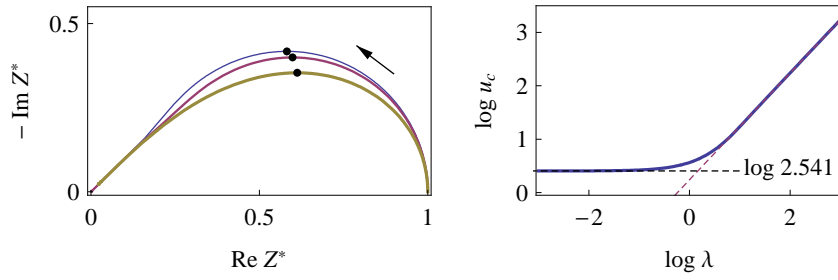


Figure 3.6: Diffusion-reaction reduced impedance #1.  $\lambda = 10^{-3}, 1, 10^3$ . Line thickness increases with  $\lambda$ .  $u_c = 2.542, 3.657, 1732$ . Change of  $\log u_c$  with  $\log \lambda$  for the diffusion-reaction reduced impedance #1.  $\lambda \rightarrow 0 \Rightarrow u_c \rightarrow 2.54, \lambda \rightarrow \infty \Rightarrow u_c \approx \lambda\sqrt{3}$ .

$$\operatorname{Re} Z^*(u) = \frac{\sqrt{\lambda} \coth(\sqrt{\lambda}) \left( \sinh(2(u^2 + \lambda^2)^{\frac{1}{4}} ca_{u\lambda}) ca_{u\lambda} + \sin(2(u^2 + \lambda^2)^{\frac{1}{4}} sa_{u\lambda}) sa_{u\lambda} \right)}{(u^2 + \lambda^2)^{\frac{1}{4}} \left( \cos(2(u^2 + \lambda^2)^{\frac{1}{4}} sa_{u\lambda}) + \cosh(2(u^2 + \lambda^2)^{\frac{1}{4}} ca_{u\lambda}) \right)}$$

$$ca_{u\lambda} = \cos\left(\frac{\arctan\left(\frac{u}{\lambda}\right)}{2}\right), \quad sa_{u\lambda} = \sin\left(\frac{\arctan\left(\frac{u}{\lambda}\right)}{2}\right)$$

$$\operatorname{Im} Z^*(u) = \frac{\sqrt{\lambda} \coth(\sqrt{\lambda}) \left( \sin(2(u^2 + \lambda^2)^{\frac{1}{4}} sa_{u\lambda}) ca_{u\lambda} - \sinh(2(u^2 + \lambda^2)^{\frac{1}{4}} ca_{u\lambda}) sa_{u\lambda} \right)}{(u^2 + \lambda^2)^{\frac{1}{4}} \left( \cos(2(u^2 + \lambda^2)^{\frac{1}{4}} sa_{u\lambda}) + \cosh(2(u^2 + \lambda^2)^{\frac{1}{4}} ca_{u\lambda}) \right)}$$

### 3.2.2 Reduced impedance #2

$$Z^*(u) = \frac{\sqrt{\lambda} \coth \sqrt{\lambda} \tanh \sqrt{(1 + i u) \lambda}}{\sqrt{(1 + i u) \lambda}}$$

$$\lim_{u \rightarrow 0} Z^*(u) = 1, \quad \lim_{u \rightarrow \infty} \sqrt{(1 + i u) \lambda} Z^*(u) = \sqrt{\lambda} \coth \sqrt{\lambda}$$

$$\lim_{\lambda \rightarrow 0} Z^*(u) = Z_{W\delta}(u/\lambda) = \frac{\tanh \sqrt{i u/\lambda}}{\sqrt{i u/\lambda}}, \quad \lim_{\lambda \rightarrow \infty} Z^*(u) = Z_G^*(u) = \frac{1}{\sqrt{1 + i u}}$$

$$\operatorname{Re} Z^*(u) = \frac{\coth(\sqrt{\lambda}) \left( \sinh(2(1 + u^2)^{\frac{1}{4}} \sqrt{\lambda} ca_u) ca_u + \sin(2(1 + u^2)^{\frac{1}{4}} \sqrt{\lambda} sa_u) sa_u \right)}{(1 + u^2)^{\frac{1}{4}} \left( \cos(2(1 + u^2)^{\frac{1}{4}} \sqrt{\lambda} sa_u) + \cosh(2(1 + u^2)^{\frac{1}{4}} \sqrt{\lambda} ca_u) \right)}$$

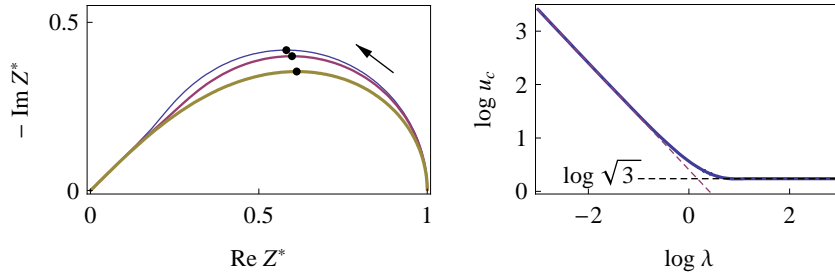


Figure 3.7: Diffusion-reaction reduced impedance #2.  $\lambda = 10^{-4}, 1, 10^3$ . Line thickness increases with  $\lambda$ .  $u_c = 25407, 3.657, 1.732$ . Change of  $\log u_c$  with  $\log \lambda$  for the diffusion-reaction reduced impedance #2.  $\lambda \rightarrow 0 \Rightarrow u_c \approx 1/(2.54 \lambda)$ ,  $\lambda \rightarrow \infty \Rightarrow u_c \rightarrow \sqrt{3}$ .

$$ca_u = \cos\left(\frac{\arctan(u)}{2}\right), \quad sa_u = \sin\left(\frac{\arctan(u)}{2}\right)$$

$$\text{Im } Z^*(u) = \frac{\coth(\sqrt{\lambda}) \left( \sin(2(1+u^2)^{\frac{1}{4}} \sqrt{\lambda} sa_u) ca_u - \sinh(2(1+u^2)^{\frac{1}{4}} \sqrt{\lambda} ca_u) sa_u \right)}{(1+u^2)^{\frac{1}{4}} \left( \cos(2(1+u^2)^{\frac{1}{4}} \sqrt{\lambda} sa_u) + \cosh(2(1+u^2)^{\frac{1}{4}} \sqrt{\lambda} ca_u) \right)}$$



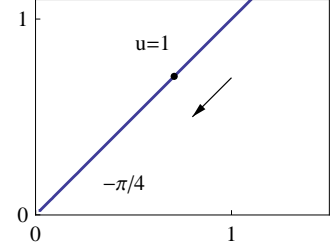
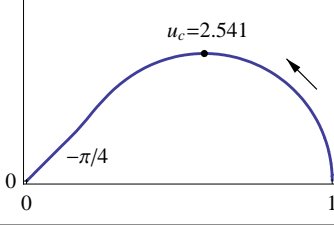
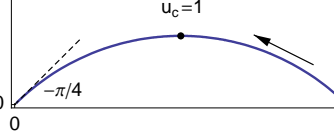
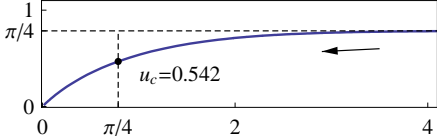
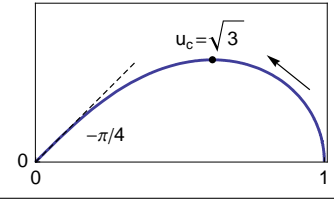
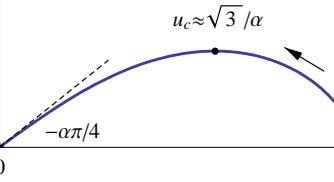


Chapter 4

Appendix

## 4.1 Table bounded diffusion and diffusion-reaction impedance

Table 4.1: Bounded diffusion and diffusion-reaction impedance.

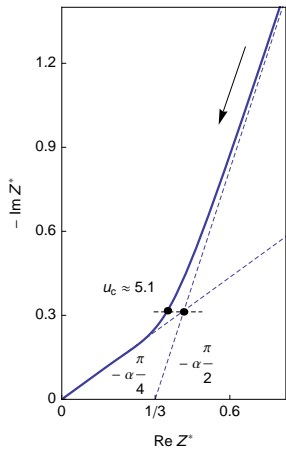
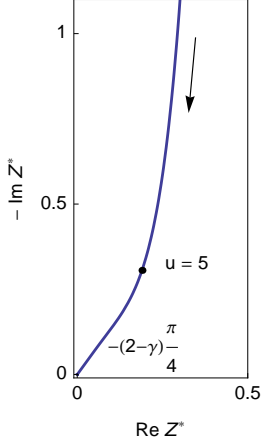
Denomination	Reduced impedance	Nyquist impedance diagram
Warburg	$Z_W^* = \frac{1}{\sqrt{i}u}$	
Bounded diffusion	$Z_{W_\delta}^* = \frac{\tanh \sqrt{i}u}{\sqrt{i}u}$	
Semi-∞ spherical diffusion	$Z^* = \frac{1}{1 + \sqrt{i}u}$	
Semi-∞ cylindrical diffusion	$Z^* = \frac{K_0(\sqrt{i}u)}{\sqrt{i}u K_1(\sqrt{i}u)}$	
Gerischer	$Z_G^* = \frac{1}{\sqrt{1 + i}u}$	
Modified Gerischer	$Z_{G\alpha}^* = \frac{1}{\sqrt{1 + (i)u}^\alpha}$	

## 4.2 Table restricted diffusion impedance

Table 4.2: Restricted diffusion impedance.

Denomination	Reduced impedance	Nyquist impedance diagram
Restricted linear diffusion	$Z_{M\delta,1}^* = \frac{\coth \sqrt{i u}}{\sqrt{i u}}$	
Restricted cylindrical diffusion	$Z_{M\delta,2}^* = \frac{I_0(\sqrt{i u})}{\sqrt{i u} I_1(\sqrt{i u})}$	
Restricted spherical diffusion	$Z_{M\delta,3}^* = \frac{1}{-1 + \sqrt{i u} \coth \sqrt{i u}}$	

Table 4.3: Restricted diffusion impedance/continued.

Denomination	Reduced impedance	Nyquist impedance diagram
Modified linear restricted diffusion	$Z^* = \frac{\coth(iu)^{\alpha/2}}{(iu)^{\alpha/2}}$	
Anomalous linear restricted diffusion	$Z^* = \frac{\coth(iu)^{\gamma/2}}{(iu)^{1-\gamma/2}}$	

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